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A gradient descent control for output tracking of a class of non-minimum phase nonlinear systems

Khalil Jouili*, Naceur Benhadj Braiek

Laboratory of Advanced Systems Polytechnic School of Tunisia (EPT), B.P. 743, 2078 Marsa, Tunisia

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Abstract

In this paper we present a new approach to design the input control to track the output of a non-minimum phase nonlinear system. Therefore, a cascade control scheme that combines input–output feedback linearization and gradient descent control method is proposed. Therein, input–output feedback linearization forms the inner loop that compensates the nonlinearities in the input–output behavior, and gradient descent control forms the outer loop that is used to stabilize the internal dynamics. Exponential stability of the cascade-control scheme is provided using singular perturbation theory. Finally, numerical simulation results are presented to illustrate the effectiveness of the proposed cascade control scheme.

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Keywords: Input–output feedback linearization; Non-minimum phase system; Singular perturbed system; Gradient descent control

1. Introduction

The control of nonlinear non-minimum phase systems is a challenging problem in control theory and has been an active research area for the last few decades. This technique, as a matter of fact, was successfully established in various practical applications (Bahrami, Ebrahimi, & Asadi, 2013; Cannon, Bacic, & Kouvaritakis, 2006; Charfeddine, Jouili, Jerbi, & Benhadj Braiek, 2010; Jouili & BenHadj, 2015; Sun, Li, Gao, Yang, & Zhao, 2016). This system control is a delicate task owing to the fact that it is a nonlinear system with non-minimum phase, and that it is also characterized by a dynamic prone to the instability of the dynamics of zero (Jouili & Jerbi, 2009; Jouili, Jerbi, & Benhadj Braiek, 2010; Kazantzis, 2004; Naiborhu, Firman, & Mu'tamar, 2013). In fact there exist no generic methods for controller synthesis and design (Khalil, 2002). Several fundamental methods in the output tracking problems on nonlinear non-minimum phase systems have been proposed in this area.

Hirschorn and Davis (1998), Isidori (1995), and Hu et al. (2015) have proposed the stable inversion method to the tracking problem with unstable zero dynamics. This method tries to find a stable solution for the full state space trajectory by steering from the unstable zero dynamics manifold to the stable zero dynamics manifold.

Khalil (2002) has derived a minimum phase approximation to a single-input single-output nonlinear, non-minimum phase system. An input–output linearizing controller is designed for this approximation and then applied to the non-minimum phase plant. This leads to a system that is internally stable. Naiborhu and Shimizu (2000) presented a controller designed based upon an internal equilibrium manifold where this controller pushes the state of a nonlinear non-minimum phase system toward that manifold. This has afforded approximate output tracking for nonlinear non-minimum phase systems while maintaining internal stability.

Kravaris and Soroush have developed several results on the approximate linearization of non minimum phase systems (Kanter, Soroush, & Seider, 2001; Kravaris & Daoutidis, 1992; Kravaris, Daoutidis, & Wright, 1994; Soroush & Kravaris, 1996). For instance Kanter et al. (2001) and Kravaris et al. (1994) investigated the system output which is differentiated as many times as the order of the system where the input derivatives

* Corresponding author.

E-mail address: khalil.jouili@gmail.com (K. Jouili).

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Nomenclature

x	vector of state variables
u	control input
y	output variable
ξ	vector of slow state variables
η	vector of fast state variables of the internal dynamics
u^*	local minimal point of a control variable u
y	scalar output
y_{ref}	reference trajectory for the output
Z	state vector of reduced subsystem
η_{ref}	virtual desired output
u_{QSS}	QSS control input
u_{ar}	artificial input
$V(x)$	Lyapunov function
$\Upsilon(u)$	performance function of a control variable u
$\psi(Z)$	descent function

that appear in the control law are set to zero when computing the state feedback input. Bortoff (1997) has studied the system input–output feedback of the first linearized. Then, the zero dynamics is factorized into stable and unstable parts. The unstable part is approximately linear and independent of the coordinates of the stable part. Charfeddine, Jouili, and Benhadj Braiek (2015) dismissed a part of the system dynamics in order to make the approximate system input-state feedback linearizable. The neglected part is then considered as a perturbation part that vanishes at the origin. Next, a linear controller is designed to control the approximate system.

Moreover, an original technique of control based on an approximation of the method of exact input–output linearization, was proposed in the works (Charfeddine, Jouili, Jerbi, & Benhadj Braiek, 2011; Guardabassi & Savaresi, 2001; Guemghar, Srinivasan, Mullhaupt, & Bonvin, 2002; Hauser, Sastry, & Kokotovic, 1992). The approximation (Charfeddine et al., 2011) is used to improve the desired control performance. A cascade control scheme has been considered (Charfeddine, Jouili, & Benhadj Braiek, 2014; Yakoub, Charfeddine, Jouili, & Benhadj Braiek, 2013) that combines the input–output feedback linearization and the backstepping approach.

On the other hand, Firman, Naiborhu, and Saragih (2015) have applied the modified steepest descent control for that system output will be redefined such that the system becomes minimum phase with respect to a new output.

In this paper, we address the problem of tracking control of a single-input single-output of non-minimum phase nonlinear systems. The idea here is to transform the given system into Byrnes–Isidori normal form, then to use the singular perturbed theory in which a time-scale separation is artificially introduced through the use of a state feedback with a high-gain for the linearized part. The gradient descent control method (Naiborhu & Shimizu, 2000) is introduced to generate a reference trajectory for stabilizing the internal dynamics.

This results in a cascade control scheme, where the outer loop consists of a gradient descent control of the internal dynamics, and the inner loop is the input–output feedback linearization.

The stability analysis of the cascade control scheme is provided using results of singular-perturbation theory (Khalil, 2002).

The rest of this paper is organized as follows. In Section 2, some mathematical preliminaries are presented. The proposed cascade control scheme and the stability analysis are given in Sections 3 and 4, respectively. In Section 5, the effectiveness of the proposed control scheme is illustrated by numerical examples. Finally, this paper will be closed by a conclusion and a future works presentation.

2. Theoretical background

In this paper, we consider a single-input single-output nonlinear system of the form:

$$\begin{cases} \dot{x} = f(x) + g(x)u \\ y = h(x) \end{cases} \quad (1)$$

where $x \in \mathfrak{R}^n$ is the n -dimensional state variables, $u \in \mathfrak{R}$ is a scalar manipulate input and $y \in \mathfrak{R}$ is a scalar output. $f(\cdot)$, $g(\cdot)$ and $h(\cdot)$ are smooth functions describing the system dynamics.

2.1. Exact input–output feedback linearization

The input output linearization is based on two concepts: the concept of relative degree and the concept of state transformation.

The relative degree r of the system (1) is defined as the number of derivation of the output y needed to appear in the input u , such as $\forall x \in \mathfrak{R}^n$:

$$\begin{cases} L_f^k h(x) = 0 \quad \forall \quad 1 \leq k \leq r-1 \\ L_g L_f^{(r-1)} h(x) \neq 0 \end{cases} \quad (2)$$

If $r \leq n$, then system (1) can be feedback linearized into Byrnes–Isidori normal form (Isidori, 1995) using the following steps:

Step 1: We apply the following control law

$$u(x) = \frac{v - L_f^r h(x)}{L_g L_f^{r-1} h(x)} \quad (3)$$

with $v = y^{(r)}$

This control law compensates the nonlinearities in the input–output behavior.

Step 2: First, system (1) is transformed into normal form (Isidori, 1995) through a nonlinear change of coordinates:

$$T(x) = \begin{bmatrix} h(x) \\ L_f h(x) \\ \vdots \\ L_f^r h(x) \\ \xi_1(x) \\ \vdots \\ \xi_{n-r}(x) \end{bmatrix} \tag{4}$$

with:

$$L_g \eta_i(x) = 0, \quad i = 1, \dots, n - r \tag{5}$$

The resulting system with the transformed variables (4) can then be written as

$$\begin{cases} \dot{\xi}_i = \xi_{i+1}, i = 1, \dots, r - 1 \\ \dot{\xi}_r = L_f^r h(x) + L_g L_f^{r-1} h(x)u \\ \dot{\eta} = Q(\xi, \eta) \\ y = \xi_1 \end{cases} \tag{6}$$

where η is the state vector of the internal dynamics.

2.2. Singular perturbed system

A singularly perturbed system is a system that exhibits a two-time scale behavior, i.e. it has slow and fast dynamics, and it is modeled as follows (Glielmo & Corless, 2010):

$$\begin{cases} \varepsilon \dot{\xi} = F_2(\xi, \eta, u, \varepsilon), \quad \xi(0) = \xi_0 \\ \dot{\eta} = F_1(\xi, \eta, u, \varepsilon), \quad \eta(0) = \eta_0 \\ y = h(x) \end{cases} \tag{7}$$

where $\xi \in \mathfrak{R}^P$ and $\eta \in \mathfrak{R}^m$ are respectively the slow and fast variables and $\varepsilon > 0$ is a small positive parameter. The functions $F_1(\cdot)$ and $F_2(\cdot)$ are assumed to be continuously differentiable.

ξ_0 and η_0 are respectively the initial conditions of the vectors ξ and η . If $\varepsilon \rightarrow 0$, the dynamics of ξ acts quickly and leads to a time-scale separation. Such a separation can either represent the physics of the system or can be artificially created by the use of high-gain controllers.

As $\varepsilon \rightarrow 0$, ξ can be approximated by its Quasi Steady State $\bar{\xi} = \vartheta(\eta, u)$ obtained by solving

$$f_1(\eta, \xi, 0) + g_1(\eta, \xi, 0)u = 0 \tag{8}$$

So, the reduced (slow) system is given by:

$$\begin{cases} \dot{\eta} = f_2(\eta, \vartheta(\eta, u), 0) + g_2(\eta, \vartheta(\eta, u), 0)u \\ = \bar{F}_2(\eta, u) \end{cases} \tag{9}$$

Note that the reduced system (8) is not necessarily affine in input.

In the next theorem, we establish the exponential stability of the singular perturbed system (7).

Theorem 1 (Khalil, 2002). Assume that the following conditions are satisfied:

- The origin is an equilibrium point for (7),
- $\vartheta(\eta, u)$ has a unique solution,
- The functions $f_1, f_2, g_1, g_2, \vartheta$ and their partial derivatives up to order 2 are bounded for ξ in the neighborhood of $\bar{\xi}$,
- The origin of the boundary-layer system (7) is exponentially stable for all η ,
- The origin of the reduced system (9) is exponentially stable.

Then, there exists $\varepsilon^* > 0$ such that, for all $\varepsilon < \varepsilon^*$, the origin of (7) is exponentially stable.

Theorem 2 (Khalil, 2002). Given system (1), if there exists a Lyapunov function $V(x)$ and positive constants χ_1, χ_2 and χ_3 such that $\chi_1 \|x\|^2 \leq V(x) \leq \chi_2 \|x\|^2$ and $\dot{V}(x) \leq -\chi_3 \|x\|^2$, then the origin is exponentially stable.

2.3. Basic results on the trajectory following method

The trajectory following method (Naiborhu & Shimizu, 2000) is a numerical optimization method based on solving continuous differential equations.

The basic idea behind a “trajectory following” method is to form a set of differential equations from the gradient of the cost function.

Consider first the minimizing problem of the form:

$$\text{minimize } \mathcal{Y}(u) \tag{10}$$

subject to no constraints

where $\mathcal{Y}(u)$ is a performance function of a control variable u .

Suppose that we use the local minimal point u^* as an initial condition for integrating the differential equation,

$$\dot{u} = \Lambda(u) \tag{11}$$

where $\Lambda(\cdot)$ is a function at our disposal, to be determined shortly.

Calculate the time derivative of $\mathcal{Y}(u)$ along the trajectory generated by the solution to (11). Then at $u = u^*$:

$$\left. \frac{\partial \mathcal{Y}}{\partial t} \right|_{u^*} = \left. \frac{\partial \mathcal{Y}}{\partial u} \right|_{u^*} \Lambda(u^*) \geq 0 \tag{12}$$

Since we are interested in a trajectory that will search a minimum, the above observation suggests that we integrate (11) by choosing

$$\Lambda(u) = - \left[\frac{\partial \mathcal{Y}}{\partial u} \right]^T \tag{13}$$

and Eq. (12) becomes

$$\frac{d\mathcal{Y}}{dt} = \frac{\partial \mathcal{Y}}{\partial u} \Lambda(u) < 0, \quad \forall u \neq u^* \tag{14}$$

Thus, in order to solve the problem of minimizing $\mathcal{Y}(\cdot)$ in an unconstrained control space, one need only to choose an appropriate initial condition for u and integrate

$$\dot{u} = - \left[\frac{\partial \mathcal{Y}}{\partial u} \right]^T \tag{15}$$

until the equilibrium solution is achieved.

3. Synthesis of the proposed control scheme

In this section, a cascade control scheme for the tracking control problem of nonlinear non-minimum phase systems is proposed. The idea of the control scheme is to use the input–output feedback linearization in the inner loop and the gradient descent control in the outer loop. The input–output feedback linearization can be seen as a pre-compensator prior to applying gradient descent control, whereas gradient descent control can be viewed as a systematic way of controlling the internal dynamics. The following control structure is proposed (Fig. 1).

3.1. Boundary layer subsystem

Consider the nonlinear system described by (1), then we apply the control law (3) which is given by:

$$\begin{cases} v = y^{(r)} \\ v = y_{ref}^{(r)} + \sum_{i=0}^{r-1} \bar{k}_{i+1} (y_{ref} - y)^{(i)} \end{cases} \tag{16}$$

with $\bar{k}_{i+1} = \frac{k_{i+1}}{\varepsilon^{r-i}}$

where y_{ref} is the reference trajectory for the output, $\varepsilon \rightarrow 0$ a small positive parameter, and $k_i > 0, \forall i \in \{1, 2, \dots, n-1\}$ are the coefficients of a Hurwitz polynomial (Isidori, 1995) and the internal dynamics are given by:

$$\dot{\eta} = Q(\eta, y, \dot{y}, \dots, y^{(r-1)}) \tag{17}$$

Under the assumption that the gains \bar{k}_i are chosen large, such as for any choice of $\varepsilon > 0$, the closed loop is stable and ε can be used as a single tuning parameter, the system (16) and (17) can be written in the form of a singular perturbed system (7). So the fast state can be defined by:

$$\xi_i = \varepsilon^{i-1} y^{(i-1)}, \quad i = 1, \dots, r \tag{18}$$

If we replace (18) by (17), we obtain

$$\begin{cases} \dot{\eta} = Q(\eta, \xi) \\ \eta(0) = \eta_0 \end{cases} \tag{19}$$

and also by (16), such that

$$\varepsilon \dot{\xi}_r = \varepsilon^r y_{ref}^{(r)} + \sum_{i=0}^{r-1} k_{i+1} (\xi_{(i+1)ref} - \xi_{i+1}) \tag{20}$$

with $\xi_{ref} = [y_{ref} \quad \varepsilon \dot{y}_{ref} \quad \varepsilon^2 \ddot{y}_{ref} \quad \dots \quad \varepsilon^r y_{ref}^{(r-1)}]^T$

thus, (17) can be written as follows:

$$\begin{cases} \varepsilon \dot{\xi}_i = \xi_{i+1}, & i = 1, \dots, r-1 \\ \varepsilon \dot{\xi}_r = \varepsilon^r y_{ref}^{(r)} + \sum_{i=0}^{r-1} k_{i+1} (\xi_{(i+1)ref} - \xi_{i+1}) \end{cases} \tag{21}$$

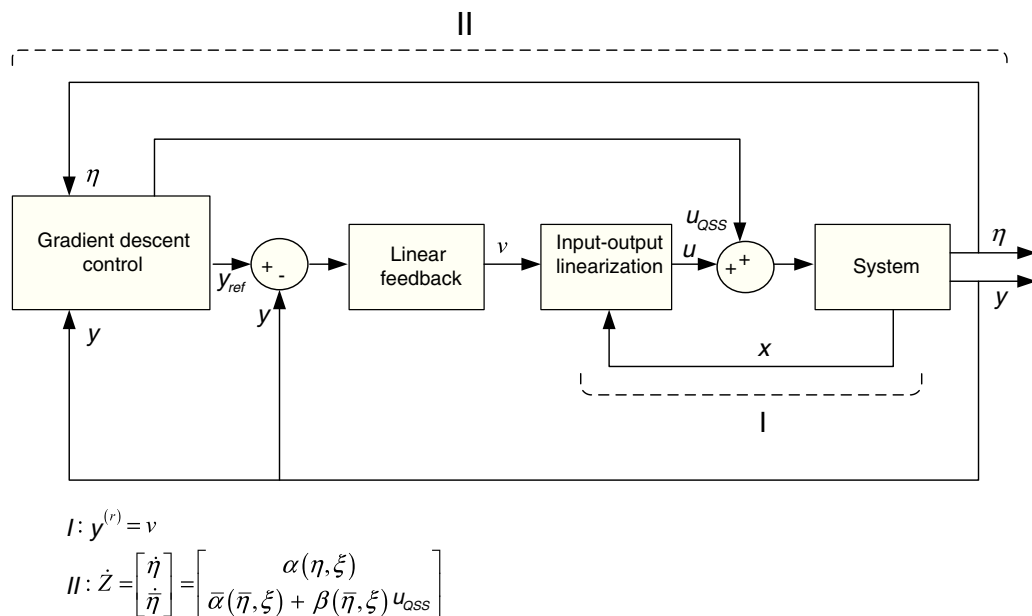


Fig. 1. Cascade control scheme using input–output feedback linearization and gradient descent control.

3.2. Reduced subsystem

The internal dynamics depends on the output y and its derivatives $\dot{y}, \dots, y^{(r-1)}$, such as:

$$\begin{cases} \dot{\eta} = Q(\eta, \xi) \\ \quad = Q(\eta, \dot{y}, \dots, y^{(r-1)}) \\ \eta(0) = \eta_0 \end{cases} \quad (22)$$

In general, the input output linearization techniques decouple between the input–output behavior y and the internal dynamics η . On the other hand, the QSS assumption decouples between the internal dynamics η and the input output behavior y . Thus, y does not have any effect on η . Therefore, the output $y^{(r)}$ is used for the control of the internal dynamics. Thus, the boundary layer subsystem (21) and the reduced subsystem (22) can be manipulated separately.

Firstly, we define a novel state vector:

$$Z = \begin{bmatrix} \eta \\ \bar{\eta} \\ y \end{bmatrix} = \begin{bmatrix} \eta_1 \\ \vdots \\ \eta_{n-r} \\ y \\ \vdots \\ y^{(r-1)} \end{bmatrix} \quad (23)$$

$$\psi(Z) = \psi \left(\eta_1, \dot{\eta}_1, \dots, \eta_1^{\gamma_\eta^1}, \dots, \eta_{(n-r)}, \dot{\eta}_{(n-r)}, \dots, \eta_{(n-r)}^{\gamma_\eta^{(n-r)}}, y, \dot{y}, \dots, y^{(r)} \right) \quad (27)$$

Such as the reduced subsystem (22) can be written by:

$$\begin{cases} \dot{Z} = \bar{Q}(Z, u_{QSS}) \\ u_{QSS} = y^{(r)} \end{cases} \quad (24)$$

The system (24) will be expressed by the following state equation:

$$\dot{Z} = \begin{bmatrix} \dot{\eta} \\ \dot{\bar{\eta}} \end{bmatrix} = \begin{bmatrix} \alpha(\eta, \xi) \\ \bar{\alpha}(\bar{\eta}, \xi) + \beta(\bar{\eta}, \xi)u_{QSS} \end{bmatrix} \quad (25)$$

where

$$\begin{cases} \eta = [\eta_1 \ \eta_2 \ \dots \ \eta_{n-r}]^T \\ \bar{\eta} = [\bar{\eta}_1 \ \bar{\eta}_2 \ \dots \ \bar{\eta}_r]^T \\ \alpha(\eta, \xi) = [\alpha_1(\eta, \xi) \ \alpha_2(\eta, \xi) \ \dots \ \alpha_{n-r}(\eta, \xi)]^T \\ \bar{\alpha}(\bar{\eta}, \xi) = [\bar{\alpha}_1(\bar{\eta}, \xi) \ \bar{\alpha}_2(\bar{\eta}, \xi) \ \dots \ \bar{\alpha}_r(\bar{\eta}, \xi)]^T \\ \beta(\bar{\eta}, \xi) = [0 \ 0 \ \dots \ 1]^T \end{cases}$$

The stability of the internal state η is required to guarantee the output system y tracks the reference output trajectory y_{ref} .

Based on the gradient descent control algorithm, we propose a method to make the internal state η tend to η_{ref} , $\eta \rightarrow \eta_{ref}$ if $t \rightarrow \infty$ (internal state regulation).

Let η be a virtual output of the system and η_{ref} be the virtual desired output.

Then we find γ_η as relative degree of the system if η is the output of the system (1). We know that $\eta \in R^{(n-r)}$ then $\gamma_\eta = [\gamma_\eta^1 \ \gamma_\eta^2 \ \dots \ \gamma_\eta^{(n-r)}]$. Based on Z and their derivatives, we construct the performance index as a descent function as follows

$$\begin{aligned} \psi(Z) = & \sum_{i=1}^{(n-r)} \left(\sum_{j=0}^{\gamma_\eta^i} b_j^i \left(\eta_{ref(i)}^{(j)} - \eta_i^{(j)} \right) \right)^2 \\ & + \left(\sum_{j=0}^r a_j \left(y_{ref}^{(j)} - \bar{\eta}^{(j)} \right) \right)^2 \end{aligned} \quad (26)$$

where the constants $a_0, a_1, \dots, a_r, b_0^i, b_1^i, \dots, b_{\gamma_\eta^i}^i, i=1, \dots, (n-r)$ will be chosen later.

Reasons why we define the descent function as in (26) are:

- i. The input u_{QSS} can be designed if there exists an explicit relationship between the input u_{QSS} and the output y . Thus, descent function (26) must be a function of $[\eta^{\gamma_\eta^1}, \dots, \eta^{\gamma_\eta^{(n-r)}}, y, \dots, y^{(r-1)}]$.
- ii. We need that the descent function:

be a quadratic form and that $\psi(0)$ be equal to zero. Accordingly, the minimum value of the descent function $\psi_0(Z)$ is zero.

If $\psi(Z)$ is zero, each term in the right side of Eq. (26) is positive $\forall t$, therefore we have:

$$\begin{cases} \sum_{j=0}^r a_j \left(y_{ref}^{(j)} - \bar{\eta}^{(j)} \right) = 0 \\ \sum_{j=0}^{\gamma_\eta^1} b_j^1 \left(\eta_{ref(1)}^{(j)} - \eta_1^{(j)} \right) = 0 \\ \vdots \\ \sum_{j=0}^{\gamma_\eta^{(n-r)}} b_j^{(n-r)} \left(\eta_{ref(n-r)}^{(j)} - \eta_{(n-r)}^{(j)} \right) = 0 \end{cases} \quad (28)$$

By choosing the values of a_0, a_1, \dots, a_r such that the Eigen values of the polynomial

$$a_r S^r + a_{(r-1)} S^{(r-1)} + \dots + a_1 S + a_0 = 0 \quad (29)$$

are real negative and the values of $b_0^i, b_1^i, \dots, b_{\gamma^i}^i, i = 1, \dots, (n - r)$ such that the Eigen values of the polynomial

$$b_{\gamma^i}^i S^{\gamma^i} + b_{(\gamma^i-1)}^i S^{(\gamma^i-1)} + \dots + b_1^i S + b_0^i = 0 \tag{30}$$

are real negative, we obtain that:

$$\begin{cases} \eta \rightarrow \eta_{ref} \\ \bar{\eta} \rightarrow y_{ref} \end{cases} \tag{31}$$

if $t \rightarrow \infty$.

In other words output tracking and regulation of internal state are achieved together (Artstein, 1983). Our objective is to find a control law u_{QSS} such that the descent function $\psi(Z)$ becomes minimum. Then the output tracking problem can be written as:

$$\left\{ \begin{array}{l} \text{decrease} \\ u_{QSS} \end{array} \right. \psi(Z) \quad \text{subj. to} \quad Z = \begin{cases} \dot{\eta} \\ \dot{\bar{\eta}} \end{cases} = \begin{cases} \dot{\eta}_1 = \alpha_1(\eta, \xi) \\ \dot{\eta}_2 = \alpha_2(\eta, \xi) \\ \vdots \\ \dot{\eta}_{n-r} = \alpha_{n-r}(\eta, \xi) \\ \dot{\bar{\eta}}_1 = \bar{\alpha}_1(\bar{\eta}, \xi) \\ \dot{\bar{\eta}}_2 = \bar{\alpha}_2(\bar{\eta}, \xi) \\ \vdots \\ \dot{\bar{\eta}}_{r-1} = \bar{\alpha}_{r-1}(\bar{\eta}, \xi) \\ \dot{\bar{\eta}}_r = \bar{\alpha}_r(\bar{\eta}, \xi) + \beta(\bar{\eta}, \xi) u_{QSS} \end{cases} \tag{32}$$

In this paper, the output tracking problem (32) will be solved using the trajectory following method.

When u_{QSS} is a scalar,

$$\frac{d\psi(Z)}{du_{QSS}} = -2a_r \left(\sum_{j=0}^r a_i (y_{ref}^{(j)} - \bar{\eta}^{(j)}) \right) \left(\frac{\partial \bar{\eta}^{(r)}}{\partial u_{QSS}} \right) - 2 \sum_{i=1}^{n-r} b_{\gamma^i}^i \left(\sum_{j=0}^{\gamma^i} b_j^i (\eta_{ref(i)}^{(j)} - \eta_i^{(j)}) \right) \left(\frac{\partial \eta_i^{(\gamma^i)}}{\partial u_{QSS}} \right) \tag{33}$$

Because the relative degree of the system is well defined,

$$\left\{ \begin{array}{l} \left(\frac{\partial \eta_i^{(\gamma^i)}}{\partial u_{QSS}} \right) \neq 0 \\ \left(\frac{\partial \bar{\eta}^{(r)}}{\partial u_{QSS}} \right) \neq 0 \end{array} \right. \tag{34}$$

The necessary condition for a local minimum

$$\frac{d\psi(Z)}{du_{QSS}} = 0 \tag{35}$$

is satisfied if at the same time:

$$\begin{cases} \sum_{j=0}^r a_i (y_{ref}^{(j)} - \bar{\eta}^{(j)}) = 0 \\ \sum_{j=0}^{\gamma^i} b_j^i (\eta_{ref(i)}^{(j)} - \eta_i^{(j)}) = 0 \end{cases} \tag{36}$$

and it happens if the value of performance index $\psi(Z) = 0$.

In the following we use a numerical technique to solve the minimization problem (32) and (33) at every point of a trajectory.

The idea of the trajectory following method is to solve the numerical optimization problem only once, at the initial point of the trajectory.

For all other points x along a trajectory, the control u_{QSS} is determined from the differential equation:

$$\begin{cases} \dot{u}_{QSS} = -\frac{d\psi(Z)}{du_{QSS}} \\ \frac{d\psi(Z)}{du_{QSS}} = -2a_r \left(\sum_{j=0}^r a_i (y_{ref}^{(j)} - \bar{\eta}^{(j)}) \right) \left(\frac{\partial \bar{\eta}^{(r)}}{\partial u_{QSS}} \right) - 2 \sum_{i=1}^{n-r} b_{\gamma^i}^i \left(\sum_{j=0}^{\gamma^i} b_j^i (\eta_{ref(i)}^{(j)} - \eta_i^{(j)}) \right) \left(\frac{\partial \eta_i^{(\gamma^i)}}{\partial u_{QSS}} \right) \end{cases} \tag{37}$$

The control law in Eq. (37) is called the steepest descent control.

Calculate the time derivative of descent function (26)

$$\begin{cases} \dot{Z} = \begin{bmatrix} \dot{\eta} \\ \dot{\bar{\eta}} \end{bmatrix} = \begin{bmatrix} \alpha(\eta, \xi) \\ \bar{\alpha}(\bar{\eta}, \xi) + \beta(\bar{\eta}, \xi) u_{QSS} \end{bmatrix} \\ \frac{d\psi(Z)}{du_{QSS}} = -2a_r \left(\sum_{j=0}^r a_i (y_{ref}^{(j)} - \bar{\eta}^{(j)}) \right) \left(\frac{\partial \bar{\eta}^{(r)}}{\partial u_{QSS}} \right) - 2 \sum_{i=1}^{n-r} b_{\gamma^i}^i \left(\sum_{j=0}^{\gamma^i} b_j^i (\eta_{ref(i)}^{(j)} - \eta_i^{(j)}) \right) \left(\frac{\partial \eta_i^{(\gamma^i)}}{\partial u_{QSS}} \right) \end{cases} \tag{38}$$

we have

$$\dot{\psi}(Z) = \frac{\partial \psi}{\partial x} \dot{x} + \frac{\partial \psi}{\partial u_{QSS}} \dot{u}_{QSS} \tag{39}$$

By substituting (21) into (38), we have

$$\dot{\psi}(Z) = \frac{\partial \psi}{\partial x} \dot{x} - \left(\frac{\partial \psi}{\partial u_{QSS}} \right)^2 \tag{40}$$

From Eq. (40) we see that the value of time derivative of descent function along the trajectory of (38) cannot be guaranteed to be less than zero for $t \geq 0$. Consider the extended system

(38) and time derivative of descent function (40). We do not have a variable which can be used to push the time derivative of descent function (40) less than zero.

Now we modify the steepest descent control (38) by adding an artificial input u_{ar} . Then the extended system (38) becomes:

$$\begin{cases} \dot{Z} = \begin{bmatrix} \dot{\eta} \\ \dot{\bar{\eta}} \end{bmatrix} = \begin{bmatrix} \alpha(\eta, \xi) \\ \bar{\alpha}(\bar{\eta}, \xi) + \beta(\bar{\eta}, \xi) u_{QSS} \end{bmatrix} \\ \dot{u}_{QSS} = -\frac{\partial\psi(Z)}{\partial u_{QSS}} + u_{ar} \end{cases} \quad (41)$$

from Sontag’s formula (Sontag, 1989), we get

$$u_{ar} = \begin{cases} \frac{1}{\frac{d\psi(Z)}{du_{QSS}}} \left[-\frac{d\psi(Z)}{dx} \dot{x} - \sqrt{\left(\frac{d\psi(Z)}{dx} \dot{x}\right)^2 + \left(\frac{d\psi(Z)}{du_{QSS}}\right)^2} \right] \\ 0 \end{cases}$$

The control law in Eq. (42) is called a modified steepest descent control. A similar method using artificial input can be seen in Shimizu, Otsuka, and Naiborhu (1999).

4. Stability analysis

In this section, we use Theorem 2 of exponential stability of singular perturbed system to analyze the stability of the closed loop system. If both the reduced and the boundary layer subsystems are exponentially stable, then the combination is also exponentially stable. The following steps will be used to prove the stability of the proposed approach.

4.1. Exponential stability of the boundary layer subsystem

Let us consider the error vector given by

$$\tilde{\xi} = \xi - \xi_{ref} \quad (43)$$

Then, the boundary layer subsystem (21) becomes:

$$\begin{cases} \varepsilon \dot{\tilde{\xi}} = \varepsilon \tilde{\xi} - \varepsilon \dot{\xi}_{ref} \\ \tilde{\xi} = \begin{bmatrix} \tilde{\xi}_1 & \tilde{\xi}_2 & \dots & \sum_{i=0}^{r-1} k_{i+1} \tilde{\xi}_{i+1} \end{bmatrix}^T \end{cases} \quad (44)$$

Letting $\tau = t/\varepsilon$ yields:

$$\frac{d\tilde{\xi}}{d\tau} = A\tilde{\xi} \quad (45)$$

with A is defined by

$$A = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 1 \\ -k_1 & -k_2 & -k_3 & \dots & -k_{n-r} \end{bmatrix}$$

Using the Theorem 2, the origin $\tilde{\xi} = 0$ is exponentially stable, and the Lyapunov function is

$$V_1(\tilde{\xi}) = \frac{1}{2} \tilde{\xi}^T P \tilde{\xi} \quad (46)$$

where $A^T P + PA = -Q$ and Q is a matrix defined positive.

4.2. Exponential stability of the reduced subsystem

To analyze the stability of the reduced subsystem, we use the following proposition:

$$\begin{cases} \text{if } \frac{d\psi(Z)}{du_{QSS}} \neq 0 \\ \text{if } \frac{d\psi(Z)}{du_{QSS}} = 0 \end{cases} \quad (42)$$

Proposition 1. *If the following statements are satisfied:*

- The system (25) is stabilizable via the choice of u_{QSS}
- $(Z=0, u_{QSS}=0)$ corresponds to an equilibrium point if $\frac{d\psi(Z)}{du_{QSS}} = 0$

Assume that system (25) satisfies the following assumption.

Assumption 1. There exists a function $V_2 : \mathfrak{R}^n \rightarrow \mathfrak{R}, V_2(0) = 0$, which is continuous, positive definite and radially unbounded such that the unforced dynamic system of (25), namely $\dot{Z} = \bar{Q}(Z, 0)$ is globally asymptotically stable, i.e., $\dot{V}_2(Z, u_{QSS}) < 0, Z \neq 0$.

First we define the performance index

$$\psi(Z, u_{QSS}) = V_2(Z) + u_{QSS}^T R u_{QSS} \quad (47)$$

where R is a matrix constant, $R > 0$. Then we determine the value of u_{ar} by Sontag’s formula (Sontag, 1989) such that the extended nonlinear system:

$$\begin{cases} \dot{Z} = \bar{Q}(Z, u_{QSS}), Z(0, 0) = (0, 0) \\ \dot{u}_{QSS} = -\frac{\partial\psi(\eta, \bar{\eta})}{\partial u_{QSS}} + u_{ar}, u_{QSS}(0) = 0 \end{cases} \quad (48)$$

is asymptotically stable about $(Z, u_{QSS}) = (0, 0)$. The most important thing is to guarantee the existence of u_{ar} .

Remark 1. Consider (47). If $u_{QSS} = 0$ then $\psi(Z, u_{QSS}) = V_2(Z)$. In other words performance index becomes Lyapunov function and so we do not need to design control input u_{QSS} for only stabilizing system.

With $u_{QSS} = 0$ we can do nothing to increase the rate of convergence. However, by adding u_{QSS} to the system, we have freedom to accelerate the rate of convergence.

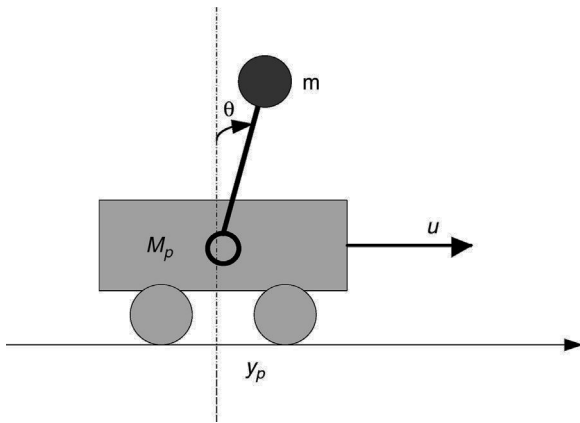


Fig. 2. Schematic diagram of the inverted cart-pendulum.

Remark 2. It would appear that when $Z=0$ is globally asymptotically stable as assumed by Assumption 1, the global stabilization of the whole system should not be difficult.

4.3. Global stability

In order to illustrate the stability of the cascade control scheme, the following exponential stability theorem is introduced.

Theorem 3. For system (1), consider a controller where u_{QSS} is obtained by solving the optimization problem (41) and the input is computed using (3). If P and R are positive definite, then there exists $\varepsilon > 0$ that would exponentially stabilize (1).

Using Theorem 1, we can conclude that there exists $\varepsilon^* > 0$ such that for all $\varepsilon < \varepsilon^*$, the origin of (1) is exponentially stable. All the conditions of theorem 1 are satisfied such that:

- The origin ($(\xi = 0), ((\eta, \bar{\eta}) = (0, 0))$) and $u_{QSS} = 0$ is an equilibrium point for the subsystems (21) and (25).
- The boundary layer subsystem (21) resulting from the QSS assumption $\varepsilon = 0$ has a unique solution y_{ref} . Also, as a result of the trajectory following method control, u_{QSS} is a function of Z .
- The origin of the boundary layer system (21) is exponentially stable $\forall Z$.
- The origin of the reduced system (25) is exponentially stable.

5. Simulation results

In this section, we will give two illustrative examples to show the applicability and efficiency of the proposed cascade control scheme. The first example is an inverted cart-pendulum system and the second one is a ball and beam system. Controlling both systems has practical importance.

5.1. Inverted cart-pendulum system

Consider the familiar inverted cart-pendulum system (Al-hiddabi, 2005), depicted in Figure 2. The cart must be moved using the force u so that the pendulum remains in the upright

Table 1
Numerical parameters of the inverted cart-pendulum system.

Notation	Description	Numerical values
M_p	Mass of the cart	0.455 kg
m	Mass of the rod	0.21 kg
L	Length of the rod	0.355 m
G	Gravitational acceleration	9.8 m/s ²

position as the cart tracks varying positions at the desired time. The differential equations describing the motion are (Al-hiddabi, 2005):

$$\begin{cases} (M_p + m)\ddot{y}_p + ml\ddot{\theta} \cos(\theta) + ml\dot{\theta}^2 \sin(\theta) = u \\ l\ddot{\theta} - \dot{y}_p \cos(\theta) - g \sin(\theta) = 0 \end{cases} \quad (49)$$

where θ is the angle of the pendulum, y_p is the displacement of the cart, and u is the control force, parallel to the rail, applied to the cart. The numerical parameters of the inverted pendulum system are given in Table 1.

Consider y_p as the output and let $x = [\theta \ \dot{\theta} \ y_p \ \dot{y}_p]^T$. The inverted cart-pendulum can be written as the system (1). Where y_p represents the output, u is the input, x is the state-space vector. Hence, one has:

$$f(x) = \begin{bmatrix} x_2 \\ \frac{1}{l} \left(g \sin(x_1) - \frac{m(lx_2^2 + g \cos(x_1)) \sin(x_1)}{M_p + m(\sin(x_1))^2} \cos(x_1) \right) \\ x_3 \\ \frac{m(lx_2^2 + g \cos(x_1)) \sin(x_1)}{M_p + m(\sin(x_1))^2} \end{bmatrix}$$

$$g(x) = \begin{bmatrix} 0 \\ \frac{\cos(x_1)}{M_p + m(\sin(x_1))^2} \\ 0 \\ \frac{1}{M_p + m(\sin(x_1))^2} \end{bmatrix}$$

and $h(x) = y_p$

The relative degree of the system is equal to $r=2$ which is strictly lower than the system dimension $n=4$.

Applying the procedure of input–output linearization to the system (49) of the inverted cart-pendulum, the boundary layer system is given by:

$$\begin{cases} \xi_1 = x_3 \\ \xi_2 = x_4 \end{cases} \quad (50)$$

its control is given by:

$$u = m(lx_2^2 + g \cos(x_1)) \sin(x_1) - M_p + m(\sin(x_1))^2 v \quad (51)$$

with $v = \ddot{y}_{ref} + \frac{k_2}{\varepsilon}(\dot{y}_{ref} - \dot{y}) + k_1(y_{ref} - y)$

and the internal dynamics is given by

$$\eta(x) = \begin{bmatrix} \eta_1(x) \\ \eta_2(x) \end{bmatrix} = \begin{bmatrix} x_3 \\ x_4 - \frac{\cos(x_1)}{l}x_2 \end{bmatrix} \quad (52)$$

Under the QSS assumption that $\dot{\theta} = \ddot{\theta} = v = 0$ and $\theta \rightarrow \cong 0$, $\sin(\theta) = \theta$ and $\cos(\theta) = 1$. Using Eq. (25), the reduced subsystem can be written as:

$$\dot{Z} = \begin{bmatrix} \dot{\eta}_1 = \eta_2 \\ \dot{\eta}_2 = \frac{1}{l}(g \sin(\eta_1) - \ddot{y}_{ref} \cos(\eta_1)) \\ \dot{\tilde{\eta}}_1 = \dot{\xi}_1 \\ \dot{\tilde{\eta}}_2 = u_{QSS} \end{bmatrix} \quad (53)$$

The control objective is to make the output θ track a desired reference trajectory θ_{ref} given that at the same time the displacement of the cart tracks the following trajectory:

$$y_{pref} = \begin{cases} 0 & t < 0 \\ (1 - \cos(t)) & 0 \leq t \leq 2\pi \\ 0 & 2\pi \leq t \leq 4\pi \\ -2e^{0.5(4\pi-t)} & t \geq 4\pi \end{cases} \quad (54)$$

The desired displacement (54) has smooth switching at $t=0$, $t=2\pi$ and non-smooth switching at $t=4\pi$.

The relative degree of η_1 is equal to $\gamma_{\eta}^1 = 2$ and the relative degree of η_2 is equal to $\gamma_{\eta}^2 = 1$.

By using Eq. (26), the descent function will be transformed under the following form:

$$\begin{aligned} \psi(Z) = & \left(\sum_{j=0}^2 b_j^1 (\eta_{1ref}^{(j)} - \eta_1^{(j)}) \right)^2 \\ & + \left(\sum_{j=0}^1 b_j^2 (\eta_{2ref}^{(j)} - \eta_2^{(j)}) \right)^2 \\ & + \left(\sum_{j=0}^2 a_j (y_{ref}^{(j)} - \tilde{\eta}_1^{(j)}) \right)^2 \end{aligned} \quad (55)$$

with

$$\begin{cases} y_{pref} = \begin{cases} 0 & t < 0 \\ (1 - \cos(t)) & 0 \leq t \leq 2\pi \\ 0 & 2\pi \leq t \leq 4\pi \\ -2e^{0.5(4\pi-t)} & t \geq 4\pi \end{cases} \\ \eta_{1ref} = \frac{\ddot{y}_{pref}}{g} \\ \eta_{2ref} = 0 \end{cases} \quad (56)$$

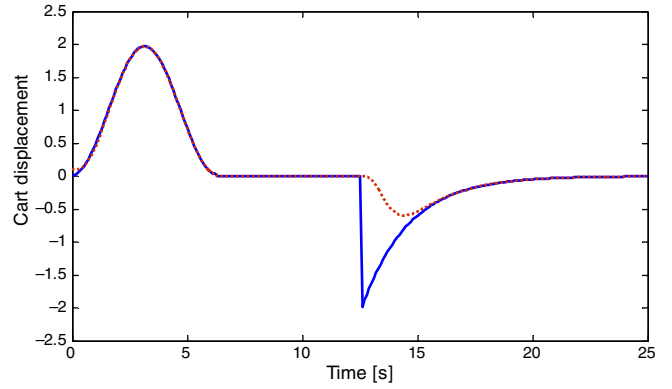


Fig. 3. Evolution of the cart displacement y_p and the reference trajectory y_{pref} (continuous line: y_{pref} , dashed line: y_p).

the input $u_{QSS} = -\frac{\partial\psi(Z)}{\partial u_{QSS}} + \frac{1}{\frac{d\psi(Z)}{du_{QSS}}}$

$\left[-\frac{d\psi(Z)}{dx} \dot{x} - \sqrt{\left(\frac{d\psi(Z)}{dx} \dot{x}\right)^2 + \left(\frac{d\psi(Z)}{du_{QSS}}\right)^2} \right]$ that stabilizes the

internal dynamics is given by solving the problem (25). In simulation, the parameters used in the input–output linearization are: $\varepsilon = 0.09$, $k_1 = 3.6$, $k_2 = 2.9$. For the gradient descent control algorithm, the employed parameters are:

$$R = \begin{bmatrix} 100 & 0 & 0 & 0 \\ 0 & 100 & 0 & 0 \\ 0 & 0 & 100 & 0 \\ 0 & 0 & 0 & 100 \end{bmatrix}, \quad P = \begin{bmatrix} 4.15 & 3.27 \\ 10.61 & 6.89 \end{bmatrix}, \quad Q = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \quad \text{and} \quad a_0 = 5.4, \quad a_1 =$$

$2.1, \quad a_2 = 3.4, \quad b_0^1 = 6, \quad b_1^1 = 9, \quad b_2^1 = 1.7, \quad b_0^2 = 2, \quad b_1^2 = 8.2$. The initial conditions are $y_p(0) = \dot{y}_p(0) = \dot{\theta}(0) = 0$ and $\theta(0) = -\pi$, the downward position for the pendulum.

The simulation results are presented by Figures 3–5. Figure 3 shows the evolution of the displacement of the cart y_p compared to the desired one y_{ref} . The simulation results in Figure 3 show

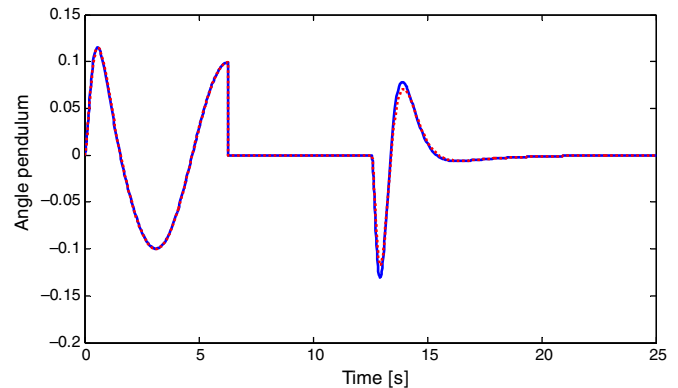


Fig. 4. Evolution of the angle of the pendulum θ and the reference trajectory θ_{ref} (continuous line: θ_{ref} , dashed line: θ).

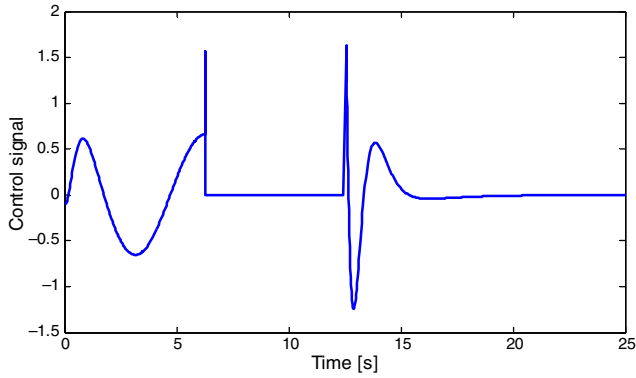


Fig. 5. Evolution of the control signal.

that the control scheme provides good tracking. In this figure, there is a perfect agreement between the two trajectories.

Figure 4 shows the evolution of the pendulum angle; indeed, it is a small variation around zero. The evolution of the stabilizing control law is shown in Figure 5. The dynamics of this control signal is quite satisfactory. In fact, there is no unacceptable physical overshoot. One can also see the reduced response time in which the control law stabilizes the controlled variable. This shows very interesting results given by the proposed cascade scheme control.

5.2. Ball and beam system

In this part, a ball and beam is considered. The ball and beam system is an unstable nonlinear system which is well known in automation; therefore, it is regarded as a perfect bench test for the design of control laws for non-minimum phase nonlinear systems.

The ball and beam system is composed of a rigid bar carrying a ball. The latter is characterized by its horizontal axis and its moment of inertia J . Its rotation angle θ compared to the horizontal one is controlled by an engine with direct current to which it applies a couple τ . A ball is placed on the beam where it is able to move with a certain freedom under the effect of gravity, as it is illustrated in Figure 6.

The dynamic model governing the behavior of the ball and beam system in open loop can be expressed by the following equations (Hauser et al., 1992):

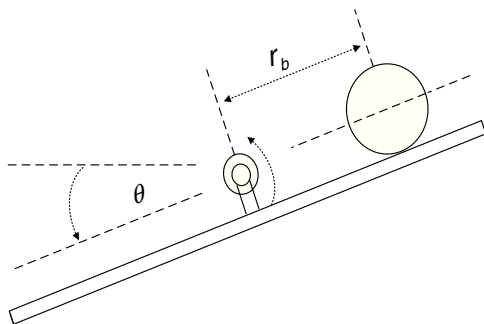


Fig. 6. Synoptic diagram of the “ball and beam” system.

Table 2
Parameters and numerical values of the ball and beam system.

Notation	Description	Numerical values
M_b	Ball mass	0.05 kg
R	Ball radius	0.01 m
J_b	Ball inertia	2×10^{-6} kg/m ²
J	Beam inertia	0.02 kg/m ²
G	Acceleration due to gravity	9.81 m/s ²
B_b	Constant	0.7143

$$\begin{cases} \left(\frac{J_b}{R_b^2} + M_b \right) \ddot{r}_b + M_b G \sin(\theta) - M_b r_b \dot{\theta}^2 = 0 \\ (M_b r_b^2 + J + J_b) \ddot{\theta} + 2M_b r_b \dot{r}_b \dot{\theta} + M_b G r_b \cos(\theta) = \tau \end{cases} \quad (57)$$

The numerical parameters of the ball and beam system are recapitulated in Table 2. To define a new input u the system can be written in state-space form as (Hauser et al., 1992):

$$\begin{cases} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \underbrace{\begin{bmatrix} x_2 \\ B_b(x_1 x_4^2 - G \sin(x_3)) \\ x_4 \\ 0 \end{bmatrix}}_{f(x)} + \underbrace{\begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}}_{g(x)} u \\ \dot{x} \\ y = x_1 \end{cases} \quad (58)$$

with

$$x = [r_b \quad \dot{r}_b \quad \theta \quad \dot{\theta}]^T, \quad y = h(x) \quad \text{and} \quad B_b = M_b / (J_b / R_b^2 + M_b).$$

The relative degree of the system is equal to $r=3$ which is strictly lower than the system dimension $n=4$.

Applying the procedure of input–output linearization to the system (58) of the ball and beam, the boundary layer system is given by:

$$\begin{cases} \xi_1 = x_1 \\ \xi_2 = x_2 \\ \xi_3 = B_b x_1 x_4^2 - B_b G \sin(x_3) \end{cases} \quad (59)$$

its control is given by:

$$u = \frac{1}{2B_b x_1 x_4} (B_b G x_4 \cos(x_3) + B_b x_2 x_4^2 + v) \quad (60)$$

with $v = \ddot{y}_{ref} + \frac{k_3}{\epsilon} (\ddot{y}_{ref} - \ddot{y}) + k_2 (\dot{y}_{ref} - \dot{y}) + k_1 (y_{ref} - y)$ and the internal dynamics is given by

$$\eta_1(x) = x_2 \quad (61)$$

Using Eq. (25), the reduced subsystem can be written as:

$$\dot{\tilde{\eta}} = \begin{bmatrix} \dot{\tilde{\eta}}_1 = \xi_2 \\ \dot{\tilde{\eta}}_2 = B_b(x_1 x_4^2 - G \sin(x_3)) \\ \dot{\tilde{\eta}}_3 = u_{QSS} \end{bmatrix} \quad (62)$$

The objective of the studied system control is to ensure that the ball always keeps contact with the beam and that its movement is carried out without slip what imposes a mechanical constraint on the acceleration of the beam. The desired trajectory is characterized by variable amplitude during time and it is given by:

$$y_{ref} = \left(1 + 0.9 \cos\left(\frac{t}{\pi}\right)\right) \cos\left(\frac{4t}{\pi}\right) \quad (63)$$

The relative degree of η_1 is equal to $\gamma_{\eta_1}^1 = 2$. By using Eq. (26), the descent function will be transformed under the following form:

$$\psi(Z) = \left(\sum_{j=0}^2 b_j^1 (\eta_{1ref}^{(j)} - \eta_1^{(j)})\right)^2 + \left(\sum_{j=0}^3 a_j (y_{ref}^{(j)} - \bar{\eta}^{(j)})\right)^2 \quad (64)$$

with

$$\begin{cases} y_{ref} = \left(1 + 0.9 \cos\left(\frac{t}{\pi}\right)\right) \cos\left(\frac{4t}{\pi}\right) \\ \eta_{1ref} = \dot{y}_{ref} \end{cases} \quad (65)$$

the input $\dot{u}_{QSS} = -\frac{\partial\psi(Z)}{\partial u_{QSS}} + \frac{1}{\frac{d\psi(Z)}{du_{QSS}}} \left[-\frac{d\psi(Z)}{dx} \dot{x} - \sqrt{\left(\frac{d\psi(Z)}{dx} \dot{x}\right)^2 + \left(\frac{d\psi(Z)}{du_{QSS}}\right)^2} \right]$ that stabilizes the internal dynamics is given by solving the problem (25). In simulation, the parameters used for the input–output linearization are: $\varepsilon = 0.098$, $k_1 = 4.8$, $k_2 = 1.7$, $k_3 = 5.3$. For the gradient descent control algorithm, the employed parameters are:

$$R = \begin{bmatrix} 70 & 0 & 0 & 0 \\ 0 & 70 & 0 & 0 \\ 0 & 0 & 70 & 0 \\ 0 & 0 & 0 & 70 \end{bmatrix}, \quad P = \begin{bmatrix} 2.33 & 11.43 & 8.43 \\ 4.21 & 8.66 & 5.63 \\ 3.22 & 1.34 & 4.88 \end{bmatrix}, \quad Q = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad \text{and}$$

$$b_0^1 = 3, \quad b_1^1 = 2.1, \quad b_2^1 = 1.5, \quad a_0 = 4, \quad a_1 = 7.2, \quad a_2 = 9.1, \quad a_3 = 3.4.$$

The result of this study is shown by Figures 7–9. Figure 7 illustrates the evolution of the tracking trajectory compared to the desired one y_{ref} . In this figure, there is an agreement between the two trajectories. The amplitude variation of the desired trajectory did not hamper the precision of the real trajectory tracking.

Figure 8 represents the beam deviation angle compared to the horizontal one which is extremely reduced in spite of the consideration of rather severe constraints of displacement.

The control signal represented by Figure 9 is characterized by a very satisfactory dynamics. This explains the important results obtained by the proposed cascade control scheme, characterized by a satisfactory bounded control signal and a better trajectory tracking. This study proves the validity of the control scheme

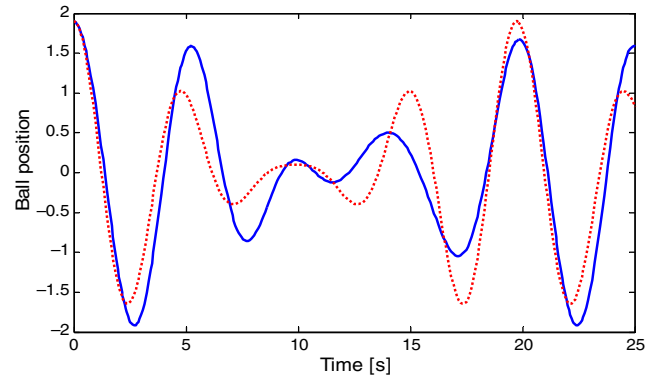


Fig. 7. Evolution of the ball position r_b and the reference trajectory y_{ref} (continuous line: y_{ref} , dashed line: r_b).

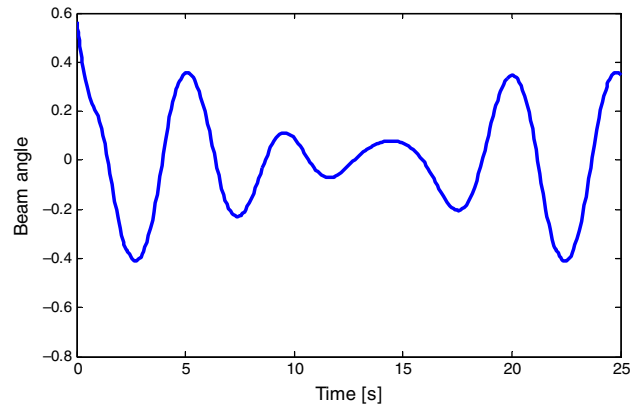


Fig. 8. Evolution of the beam angle θ .

to ensure the high performance control for the ball and beam system.

In fact, the contribution of the cascade control scheme seems to be adapted to the amplitude variation of the desired trajectory.

5.3. Discussion

The main objective of this work was the control of single-input single-output nonlinear systems, using input–output feedback linearization technique.

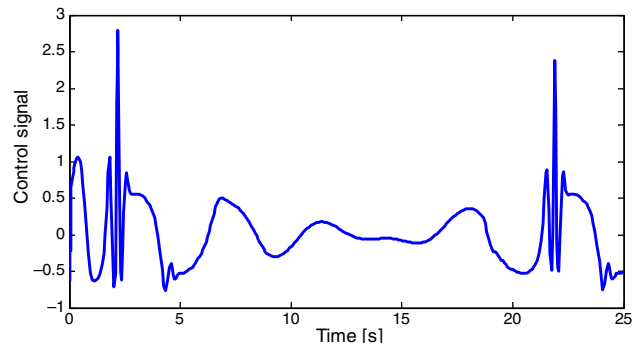


Fig. 9. Evolution of the control signal.

The proposed methodology is based on input–output feedback linearization, gradient descent control method and singular perturbation theory.

The system is first input–output feedback linearized, separating the input–output system behavior from the internal dynamics. Gradient descent control is then used to stabilize the internal dynamics, using a reference trajectory of the system output. This results in a cascade-control scheme, where the outer loop consists of a gradient descent control of the internal dynamics, and the inner loop is the input–output feedback linearization.

The stability analysis of the cascade control scheme is provided using results of singular perturbation theory. The key idea is to introduce a time-scale separation, enforced by the introduction of a small parameter in the controller. Therefore, the quasi steady state assumption is made, allowing the input–output behavior of the system to be decoupled from its internal dynamics.

Thus, each subsystem is analyzed separately, providing a stability proof of the overall system.

The main contribution of the stability analysis is the global exponential stability of the gradient descent control scheme. The use of singular perturbation theory requires exponential stability results.

Indeed, the application of this methodology to the inverted cart-pendulum and ball and beam systems has shown excellent results.

6. Conclusion

A cascade control strategy scheme for the tracking problem of non-minimum phase nonlinear systems was presented and successfully applied to the inverted cart-pendulum system and ball and beam model.

This strategy is based on the approximation of the non-minimum phase system by another singular perturbed system. The proposed controller uses the input–output linearization technique to cancel the nonlinearities of the external dynamics and to stabilize the internal dynamics by the gradient descent control algorithm. A stability analysis of the proposed approach has been provided based on the singular perturbation theory. The simulation results have shown excellent results.

Although the approximate input–output feedback linearization was developed in this work for the control of single-input single-output systems, the obtained results can be easily extended to the multi-input multi-output case. On the other hand, the robustness of the proposed approach is not studied in this paper. This could be investigated in the future work.

Conflict of interest

The authors have no conflicts of interest to declare.

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